

M80 Noise Modelling Report

3513048C

Prepared for Bilfinger RE Asset Management Ltd Pavilion 2 Buchanan Park Stepps Glasgow G33 6HZ

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EXECUTIVE SUMMARY

Highway Managemen between Stepps and	(PB) has been instructed by Bilfinger RE Asset Management Ltd on behalf of t (Scotland) Limited to undertake a noise assessment for the M80 motorway Haggs. The purpose of the assessment is to assist Highway Management discharging the following obligations as part of the O&M phase:
Schedule 2 of	the New Work Requirements.
The above schedules in the Environmental S	relate to the assessment of post-construction noise levels at properties defined Statement (ES).
computer noise mode scenarios of the sche	undertaken in August 2014 at representative locations along the scheme. A el using CadnaA was prepared for the pre-construction and post-construction eme. Noise predictions were undertaken in accordance with the methodology prandum 'Calculation of Road Traffic Noise' (CRTN).
Due construction and	next construction reside lowely and remembed for 404 rememberships reconstruction

Pre-construction and post-construction noise levels are reported for 121 representative receptors. Noise levels predicted for the post-construction scenario have been compared against the pre-construction (2008) and the ES 2010 with scheme and mitigation results.

Results of the assessment indicate that 117 locations are compliant with the contractual requirements. Of the 4 locations that are not compliant, the differences are explained by factors unrelated to the physical works on the M80 for three locations, and due to a noise barrier that was not included in the final scheme for the other location.

1 INTRODUCTION

1.1 Context

- 1.1.1 Parsons Brinckerhoff (PB) has been instructed by Bilfinger RE Asset Management Ltd on behalf of Highway Management (Scotland) Limited to undertake a noise assessment for the M80 motorway between Stepps and Haggs to assist with discharging the obligations on the Design, Build, Finance and Operate (DBFO) Contract - O&M phase. These are defined in Schedule 2 of the New Work Requirements on the scheme.
- 1.1.2 This report details the outcome of the following agreed scope of work:
 - Prepare a noise model using CadnaA and CRTN for pre-construction (2008) and post-construction (2012) scenarios of the scheme;
 - Undertake a noise survey at various locations for validation of the noise model;
 - Report the post-construction ambient noise levels (noise model) for the 121 representative noise sensitive locations given in the Environmental Statement (ES);
- 1.1.3 **Appendix A** presents a glossary of acoustic terminology.

1.2 Study Area

- 1.2.1 The study area for the noise model consists of a calculation area which is 300m either side of the new and existing roads surrounding the M80 scheme. This is the extent of validation for the CRTN prediction methodology.
- 1.2.2 It should be noted that the majority of these buildings are single dwellings comprising of two floor levels. A limited number of properties correspond to multi-storey buildings; receptors have also been included at higher floors, where applicable. The 121 noise sensitive properties assessed in the ES have been reported.

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2 LEGISLATION AND CONTRACT DOCUMENTS

2.1 Calculation of Road Traffic Noise (CRTN), 1988

- 2.1.1 This memorandum describes the methodology to calculate the road traffic noise at a given distance from the highway.
- 2.1.2 The methodology takes into account the intervening ground cover, road configuration and road layout. The calculation assumes a typical traffic and noise propagation conditions. Noise levels are presented in terms of the noise descriptor L_{A10,18h} which is the arithmetic average of the noise level exceeded for 10% of the time between 06:00 and 24:00 hours.
- 2.1.3 The variables used in the calculation of the traffic noise level are:
 - The annual average week day traffic flow (AAWT) for the 18-hour period from 06:00 to 24:00 hours;
 - Mean traffic speed;
 - Percentage of heavy vehicles;
 - Road gradient;
 - Type of road surface;
 - Distance of the receptor from the road;
 - Nature of the ground cover between the road and the receptor;
 - Screening and reflection effects.
- 2.1.4 It has been agreed with Bilfinger that the CRTN method would be used for the purposes of the modelling.

2.2 Contract Requirements

Schedule 2

- 2.2.1 The DBFO contract includes a number of clauses relating to potential noise impacts under Schedule 2. Clause 4.8 sets out the requirements for Traffic Noise and Vibration.
- 2.2.2 Paragraph 4.8.2 (i) sets out criteria to be met for noise levels due to traffic movements which upon completion of the New Works are to be no greater than those recorded in pre-construction noise survey (as per App 1/9 to Part 3 of the New Works Requirement for those parts of the scheme that are adjacent to the on-line section. For receptors adjacent to the off-line section, the ES 2010 with mitigation levels should be taken as a maximum level not to be exceeded.
- 2.2.3 Paragraph 4.8.2 (iii) requires a post-construction ambient noise assessment to be carried out to demonstrate that the Design complies with the requirements of 4.8.2. This report is presented in full compliance with this requirement.



3 METHODOLOGY

3.1 Liaison

- 3.1.1 A meeting was held on 25th February 2014 to agree on the noise survey, modelling and assessment methodologies. The following bullet points summarise the agreement:
 - The noise survey will be undertaken in accordance with the shortened measurement procedure in CRTN for the purposes of validating the CRTN noise model;
 - Four CRTN monitoring locations will be undertaken during a typical working day, as suitable weather conditions allows. Measurements will record the noise parameters L_{Aeq}, L_{A90}, L_{A10}, L_{Amax} and L_{Amin} for 3 x 1hour periods;
 - A noise model will be produced for the scheme. The model will be prepared using CadnaA and two scenarios will be created: pre-construction (2008) and post-construction (2012). The model will be based on existing noise models. Traffic data will be provided.
- 3.1.2 After the meeting, further liaison was made with the project team to discuss the information received and assumptions in the model. These are further detailed later in this report (Methodology Modelling).

3.2 Noise Survey

- 3.2.1 A survey was conducted between 19th and 20th August in accordance with the shortened measurement method (Paragraph 43) from CRTN. The results of the CRTN survey have been used to validate the road traffic noise model. The guidance and reporting requirements set out in BS7445-2:1991 *'Description and measurement of environmental noise. Guide to the acquisition of data pertinent to land use'* have also been followed. **Appendix B** presents the noise survey report detailing the methodology results and calibration certificates of the equipment used in the survey.
- 3.2.2 Short-term CRTN noise measurements were undertaken at 4 locations along the scheme, as illustrated in **Figure 1** (overleaf). One series of 3 x 1-hour measurements were conducted at each of these locations at 1.5m above ground level.
- 3.2.3 The following parameters were recorded: L_{Aeq}, L_{A90}, L_{A10}, L_{Amax} and L_{Amin} using fast time weighting and A-weighted frequency network. Measurements were made in the absence of precipitation and the wind from source to receiver was recorded as less than 3m/s as identified in **Appendix B**.



Figure 1: Noise Survey Locations



3.3 Noise Modelling

- 3.3.1 A road traffic noise model for the scheme was prepared using CadnaA. Noise predictions were undertaken following the methodology described in CRTN.
- 3.3.2 The following bullet points summarise the sources of information and assumptions used in the model. A table with a list of modelling assumptions is presented in **Appendix C** along with details of the traffic data provided by HMG for use in the assessment, and the rationale for the post processing of traffic data undertaken.
 - Building height information in the existing models was verified with satellite images and observation during the noise survey. The topographical data for the post construction (2012) model was extracted from the models produced previously, which is assumed to be based on a detailed topographical survey as part of the project. Vertical alignment data provided was used for the preconstruction (2008) model for the entire M80 scheme except for Auchenkilns junction which was taken from the relevant model.
 - For high rise buildings, the assessment assumed that there is one dwelling per floor.
 - Buildings are included in the model to account for screening effects, but the levels are calculated as free field levels, and thus a correction of 2.5 dB has been added to the modelling results at each of the receptors to convert it to a façade noise level; Some locations relate to car parks and open areas, and these are reported as free field levels.



- Where the receptor locations are near buildings they are set 1m away from facades.
- The road surface type was known to be HRA with a texture depth of 1.5mm in 2008. In 2012 the road surface of the M80 was a new low noise surface (-3.5dB). In both years the Auchenkilns Junction had a low noise surface (-2.5 dB). On all minor roads with speeds <75 km/hr a correction of -1 dB is used for both years.
- Noise barriers were included in the model as appropriate. Through liaisons with HMG, PB understands that barriers were in place at the Auchenkilns Junction in 2008, with the remainder in place by 2012;
- Traffic data for the M80 and surrounding road network was provided by HMG from actual traffic counts, and supplemented with data reported in the M80 Environmental Statement. Minor processing was made to convert the sets of data received in hourly format into Annual Average Weekly Traffic (AAWT) 18 hours format as required by CRTN. Some data has also been extrapolated to ensure a sufficient dataset was available. **Appendix C** lists the complete dataset (Road Traffic Data Table) used for the purposes of the noise modelling, and the rationale for the post processing of data. A traffic data schematic (**Figure C**) is also included for clarity.
- 3.3.3 The post-construction scenario has been validated against the results of the noise survey. Receptors have been implemented in the noise model at the same locations and height as measured during the survey. Results are presented in the next section.



4 RESULTS

4.1 Noise Survey

4.1.1 Table 1 presents the results of the noise survey in terms of the noise descriptor $L_{A10,3h}$ dB. In addition, the equivalent $L_{A10,18h}$ value has been calculated by subtracting 1dB from the 3 x 1 hour readings. The table also shows the distance from the main road to the measurement location.

Table 1: Noise Survey Result Summary

Measurement Location (ML)	Distance from road (Metres)	Measured L _{A10,3h} dB	Equivalent L _{A10,18h} dB (06:00 – 24:00)
ML2 – M73 Off slip	3	73.4	72.4
ML9 - Glenview Avenue	7	73.1	72.1
ML13 – Carrick Road	6	78.8	77.8
ML15 – Castlecary Road	10	80.0	79.0

4.2 Noise Modelling

Noise Modelling Validation

- 4.2.1 Validation of the post-construction modelling scenario for 2012 has been undertaken against the survey results from August 2014. Traffic counts and HGV percentages were obtained during the surveys to enable a correction to be applied between 2014 and 2012 to reflect the difference in traffic flows. Traffic flows on the days of the surveys (2014) were compared for each survey location with the traffic flow data in our 2012 noise model. Noise predictions were then made with the traffic data on the day of the survey as input to the model at each survey location.
- 4.2.2 The changes at each measurement location between 2014 and 2012 were:
 - ML2 M73 Offslip the 2014 flows were 11% greater than the 2012 flows but a 1% decrease in HGVs which would result in a relative change of 0.1 dB at that survey location.
 - ML9 Glenview Avenue the 2014 flows were 2% lower than the 2012 flows but a 6% increase in HGVs which would result in a relative change of 0.2 dB.
 - ML13 Carrick Road the 2014 flows were 4% greater than the 2012 flows and a 10% increase in HGVs which would result in a relative change of 0.9 dB.
 - ML15 Castlecary Road the 2014 flows were 8% greater than the 2012 flows and 4% increase in HGVs which would result in a relative change of 0.6 dB.



4.2.3 Table 2 presents a comparison of the measured data, the 2014/2012 correction and the predicted model data at each location. Positive values mean that the modelling results are higher.

Measurement Location (ML)	Noise Modelling Results L _{A10,18h} dB	Noise Survey Results L _{A10,18h} dB	Correction due to traffic flow difference between 2014 & 2012,dB	Difference (Model – Survey) dB
ML2 – M73 Off slip	73.2	72.4	0.1	0.9
ML9 - Glenview Avenue	73.2	72.1	0.2	1.3
ML13 – Carrick Road	77.8	77.8	0.9	0.9
ML15 – Castlecary Road	76.7	79.0	0.6	-1.7

Table 2: Noise Survey vs. Noise Modelling (2012) Results

4.2.4 It can be seen from Table 2 that the differences between the noise survey and the modelling results are within 1.7 dB for all locations. This is an acceptable tolerance for the purposes of the noise modelling exercise.

ES Noise Sensitive Receptors

- 4.2.5 Post-construction noise levels have been predicted at 121 sensitive receptors as identified in the ES to fulfil the obligations in Paragraph 4.8.2, Schedule 2 of the DBFO Contract. The location and name of these properties have been obtained from the 'M80 Stepps to Haggs Environmental Statement' Figure 15.1.1 to Figure 15.1.19 and Tables 15.8, 15.9 and 15.10.
- 4.2.6 **Appendix D** presents Figure D1 to D4 showing the location of the 121 receptors. A table is presented in the appendix showing the façade noise levels at all the receptors during the post-construction phase of the scheme.
- 4.2.7 Pre-construction noise levels have been also predicted at the 121 ES sensitive receptors. A table with the results is presented in **Appendix D**. The table is split into two sections listing receptors adjacent to the off-line and on-line sections respectively.
- 4.2.8 For the off-line section (Table D1 i), PB's 2012 post construction levels in the fifth column have been compared against the ES 2010 with mitigation levels in the fourth column, with the difference reported in the last column. Non-Compliant Data is highlighted in the last column in a dark red text with a light red background.
- 4.2.9 For the on-line section (Table D1 ii), the PB 2012 post construction levels in the fifth column have been compared with the 2008 (pre-construction) levels in the third column, with the difference reported in the sixth column. Non-Compliant Data is highlighted in the sixth column in a dark red text with a light red background.
- 4.2.10 Results of the assessment indicate that 117 locations are compliant with the contractual requirements. All 4 of the locations that are not complaint are on the offline section. Table 3 presents the locations that are not compliant with the contractual requirements.



Table 3: Non-Compliant Properties

· · ·				
ES Noise Sensitive Receptor locations		Contractual re	equirement	
Off-line Section properties	Floor	PB 2012 L _{A10,18h} dB	ES2010 with mitigation L _{A10,18h} dB	Difference (dB)
Crow Wood House, Cumbernauld Road	Ground floor	72.4	66.4	6.0
Muirhead, Glasgow, Strathclyde G69 9BS	1 st floor	73.5	68.7	4.8
12 Church Road,	Ground floor	75.1	64.0	11.1
Muirhead, Glasgow, Lanarkshire G69 9EB	1 st floor	76.3	66.0	10.3
13 Dunellan Avenue,	Ground floor	69.1	60.1	9.0
Moodiesburn, Glasgow, Lanarkshire G69 0GD,	1 st floor	70.3	62.0	8.3
24 Stoneyetts Cottages,	Ground floor	63.0	61.0	2.0
Muckcroft Road Glasgow, Lanarkshire G69 0JH	1 st floor	63.8	63.1	0.7

5 INVESTIGATION OF NON-COMPLIANT PROPERTIES

Off-Line Section

- 5.1.1 There are 19 off-line locations assessed in the ES. Comparison of the 2012 results with the ES 2010 predictions reveals that 4 of the 19 locations do not, at face value, achieve compliance with the contractual requirement.
- 5.1.2 The first 3 (Crow Wood House, 12 Church Road & 13 Dunellan Avenue) are properties which are adjacent to the A80, which does not form part of the M80 scheme. A reason for the discrepancy appears to be from the ES's traffic flow predictions. The ES predicts a decrease of roughly 80% in that area, while the traffic data collected reveals a decrease of roughly 40%. This accounts for the difference in levels. Therefore the difference at these properties is outside the control of the scheme.
- 5.1.3 The other off-line location, 24 Stoneyetts Cottages is situated to the north of the offline section which has an increase of 2.0 dB. PB has noticed that previous models included a noise barrier design to protect this property which was not confirmed as being installed as part of the scheme. The barrier would have provided a similar level of attenuation to the level of increase, and therefore we do not consider this property to be non-compliant.



On-Line Section

- 5.1.4 There are 102 on-line locations assessed in the ES. Comparison of the 2012 results with the pre-construction year reveals that all 102 locations achieve compliance with the contractual requirement.
- 6 CONCLUSIONS
- 6.1 Summary
- 6.1.1 A noise assessment has been undertaken at the M80 between Stepps and Haggs to determine the post-construction noise levels at 121 noise-sensitive locations defined during the Environmental Statement (ES).
- 6.1.2 Results of the assessment indicate that 117 locations are compliant with the contractual requirements. Of the 4 locations that are not compliant, the differences are explained by factors unrelated to the physical works on the M80 for three locations, and due to a noise barrier that was not included in the final scheme for the other location.

M80 Noise Modelling Report



APPENDIX A – GLOSSARY OF TERMS



Ambient Noise	The total sound in a given situation at a given time, usually composed of sound form may sources near and far.
A – Weighting	A-weighting has been found to give the best correlation between perceived and actual loudness. Measurement to which this weighting has been applied include an A in their descriptor.
Background Noise Level, L _{A90,T}	The level exceeded for 90% of a given time interval, T.
Decibel (dB)	A logarithmic unit for measuring the relative loudness of noise, i.e. the sound level.
Environmental Noise	Noise governed by environmental legislation, and usually enforced by local authorities. Also termed "nuisance".
Facade Effect	The phenomenon of sound energy (noise) being reflected form the hard rigid, external surface of a building or structure. Where a facade is present, this effect adds approximately 2.5 or 3 dB to the free field noise level (at a distance of 1 metre from the facade).
Free Field Noise Level	The noise level measured away from any reflecting surfaces.
Hertz (Hz)	Unit of frequency, equal to one cycle per second. Frequency is related to the pitch of the sound.
L _{Aeq, T}	The equivalent continuous sound level. It provides an "average" sound level over a defined period of time (T).
L _{A10, 3h}	The L _{A10} is the sound level exceeded 10 per cent of the time and it is used to define road traffic noise. The L _{A10} (3 hour) dB is the arithmetic average of the values of L _{A10} hourly dB for three one-hour periods between 1000 and 1700 hours. It is used as a way of calculating the L _{A10, 18h} using the equation: $L_{A10, 18h} = L_{A10, 3h} - 1$.
La10, 18h	The L_{A10} is the sound level exceeded 10 per cent of the time and it is used to define road traffic noise. The L_{A10} (18 hour) dB is the arithmetic average of the values of L_{A10} hourly dB for each of the eighteen one-hour periods between 0600 and 2400 hours.
L _{Amax}	The maximum sound level measured.

M80 Noise Modelling Report



APPENDIX B – NOISE SURVEY REPORT



December 2014

NOISE SURVEY REPORT

Bilfinger RE Asset Management Ltd

3513048C

Issue 2

M80 Noise Survey Report

3513048C

Prepared for Bilfinger RE Asset Management Ltd Pavilion 2 Buchanan Business Park Stepps Glasgow G33 6HZ

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1 INTRODUCTION

1.1 Background

- 1.1.1 Parsons Brinckerhoff (PB) has been commissioned by Bilfinger RE Asset Management Ltd to undertake a noise survey at the M80 between Stepps and Haggs, Glasgow.
- 1.1.2 The purpose of this report is to inform the noise climate at a number of receptors along the M80. In addition, the results of these noise measurements will be used to validate a noise model.
- 1.1.3 A noise survey was undertaken on the 19th and 20th of August 2014 in accordance with the shortened methodology advised in 'Calculation of Road Traffic Noise' (CRTN)[1] and BS7445 [2],[3].

1.2 Site Description

- 1.2.1 The noise survey was undertaken at 4 locations along the section of the M80 that runs between the town of Stepps and village of Haggs. The land use in the surrounding areas is predominantly rural, interspersed with small towns, business parks and residential areas.
- 1.2.2 **Figure A** presents the 4 measurement locations used in the survey. More detailed Figures (**B-F**) showing each location can be found in **Annex A**.

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Figure A



2 GUIDANCE

2.1 Calculation of Road Traffic Noise (CRTN)

2.1.1 The shortened measurement procedure given within Calculation of Road Traffic Noise (CRTN) has been adhered to for the measurements.

3 METHODOLOGY

3.1 Noise Surveys

- 3.1.1 All 4 measurements were attended with 1 engineer from PB mobilised to site and the measurement period was 3 hours at each location, except for measurement location ML13 where a battery failure meant that the measurement was only 2 hours and 50 minutes long. In this instance the L_{A10} was noted down for the last 50 minute period.
- 3.1.2 From discussions with Bilfinger it was agreed that free field measurements on publically accessible land would be suitable. All measurements were made using Class 1 Integrating-Averaging Sound Level Meters (SLM) as defined in International Electrotechnical Commission (IEC) 61672:2003[4].
- 3.1.3 For each measurement, the following noise parameters were recorded: L_{eq} , L_{90} , L_{10} L_{max} and L_{min} , in 1/3 octave bands. Fast time weighting and A-weighted frequency network were used.

- 3.1.4 Calibration certificates for the instrumentation used in the survey are presented in **Annex C**.
- 3.1.5 It should be noted that for the purpose of this report, emphasis is given to the results for the noise parameter L_{A10} dB, in line with Calculation of Road Traffic Noise (CRTN).
- 3.1.6 Measurement results for the CRTN shortened procedure have been given as L_{A10,3h}, which is the arithmetic average of the 3 measured L_{A10,1h} values in decibels, at each measurement location. CRTN provides an equation which converts L_{A10,3h} into L_{A10,18h}.
- 3.1.7 Measurements were made in the absence of precipitation. The wind direction from source to receiver was less than 3 m/s. A windshield was used to minimise the effects of wind-induced noise at the microphone.

4 RESULTS

- 4.1.1 **Table A** presents a summary of the noise survey results at the 4 locations. A more detailed version of the results is presented in the noise survey forms (See **Annex B**).
- 4.1.2 The equivalent $L_{A10,18h}$ was calculated by subtracting 1 dB from the measured $L_{A10,3h}$. The distance of the microphone from the edge of the nearest main road is also presented in **Table A**.
- 4.1.3 The dominant noise source at all of the locations was that of road traffic noise from the M80 scheme. Further subjective comments on the noise climate can be found in the noise monitoring forms (See **Annex B**).

Measurement Location (ML)	Distance from road (Metres)	Measured L _{A10,3h} dB(A)	Calculated L _{10,18h} dB(A) (06:00 – 24:00)
ML2(August)- M73 Off slip	3	73.4	72.4
ML9(August)- Glenview Avenue	7	73.1	72.1
ML13(August) – Carrick Road	6	78.8	77.8
ML 15(August) – Castlecary Road	10	80.0	79.0

Table A: Survey Data

5 REFERENCES

- 1. Calculation of Road Traffic Noise' (CRTN) 1988 Department of Transport, HMSO
- 2. BS 7445-1: 2003 "Description and Measurement of Environmental Noise: Guide to quantities and procedures", BSI
- 3. BS 7445-3: 1991 "Description and Measurement of Environmental Noise: Guide to application to noise limits ", BSI
- 4. IEC 61672:2003 "Electroacoustics sound level meters", BSI



ANNEX A

SURVEY MEASUREMENT LOCATIONS

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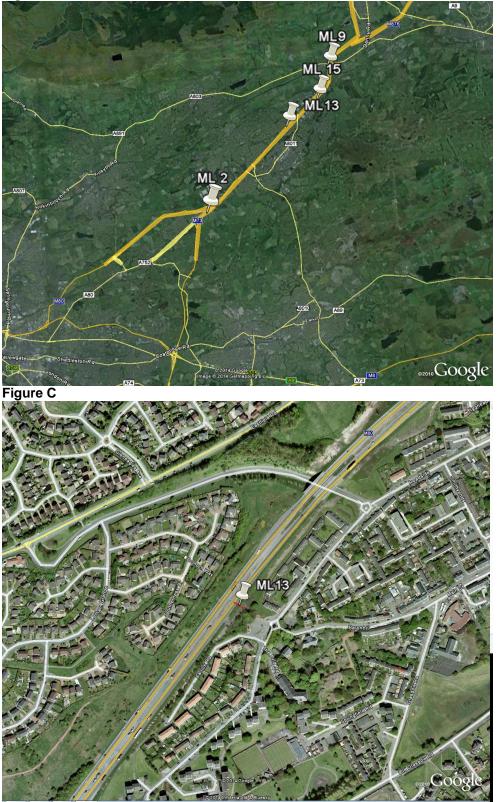


Figure D

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Figure E









Measurement Location (ML)

ML 2 – M73 Off slip

ML 9 - Glenview Avenue

ML 13 – Carrick Road

ML 15 (August)- Castlecary Road



ANNEX B

NOISE SURVEY FORMS



Noise Monitoring Fo	orm										PARSONS BRINCKERHOFF
Project:	M80 (part C)					Job Numb	per:			3513048C	
Location:	ML2 (August)										
Equipment:		NA-28				Engineer:					Adam Price
Pre-Calibration Leve	el:	94.0 dB					leather Des	scription:			Mix of clear skies and then overcast
Post-Calibration Lev	vel:	93.9 dB Date: 19/08/2014					19/08/2014				
Measi	urement Period			Weather			Statistic	al Noise Le	vels / dB		1
Date	Start Time	Elapsed Minutes	Wind Speed (m/s)	Wind Direction (from)	Tomporatu	L _{Aeq}	L _{Amax}	L _{Amin}	L _{A10}	L _{A90}	Description of Audible Noise
19/08/2014	10:00	60	0-1	SW	12	72.7	86.4	53.8	76.5	62.4	
19/08/2014	11:00	60	0-1	SW	12	72.7	86.9	58.5	76.3	63.2	(dominant) Road traffic noise, birdsong
19/08/2014	12:00	60	0-1	SW	12	73.0	87.2	57.2	76.8	62.7	
	DTS P	EL'A RAASPORT SERVICES									

M80 Noise Survey Report Issue 2 December 14 Prepared by Parsons Brinckerhoff for Bilfinger RE Asset Management Ltd

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	ing Form										PARSONS BRINCKERHOFF		
-	M80 (part					Job Nun	nber:				3513048C		
ocation:	ML13 (Au	gust)											
quipment:		NA-28				Enginee					Adam Price		
Pre-Calibration Level: 94.0 dB					-	Weather	Descrinti	on.		Mix of clear skies and then overcast			
Post-Calibration Level: 94.0 dB				Date:	Weather	Descripti	011.		19/08/2014				
	201011	01.0 42				Dutoi					10/00/2011		
Measurement Period Weather							Statistica	l Noise L	evels / dE	3			
Date Start Elapsed Wind Wind Time Minutes (m/s) (from)					L _{Amax}	L _{Amin}	L _{A10}	L _{A90}	Description of Audible Noise				
19/08/2014	14:00	60	0-1	SW	12	77.8	86.4	53.7	80.5	72.4			
19/08/2014	15:00	60	0-1	SW	12	78.0	87.9	63.5	80.4	73.7	(dominant) Road traffic noise, birdsong		
19/08/2014	16:00	60	0-1	SW	12	N/A	N/A	N/A	80*	N/A			
					and the second se	1		A -					

December 14

for Bilfinger RE Asset Management Ltd

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	oring Form	l									PARSONS BRINCKERHOI
Project:	M80 (part	C)				Job Numb	er:		3513048C		
Location:	ML9 (Augu	ist)									
Equipment:		NA-28				Engineer:					Adam Price
Pre-Calibration Level: 94.0 dB						General W	leather Des	scription:			Mix of clear skies and then overcast
Post-Calibrat	ion Level:	93.9 dB				Date:					20/08/2014
Measu	rement Pe	riod		Weather			Statistica	al Noise Le	vels / dB		
Date	Start Elapsed Speed Direction Tempe		Temperat ure (°C)	L _{Aeq}	L _{Amax}	L _{Amin}	L _{A10}	L _{A90}	Description of Audible Noise		
20/08/2014	11:00	60	0-1	SW	12	70.8	86.8	57.8	73.5	66.1	
20/08/2014	12:00	60	0-1	SW	12	70.5	82.3	52.4	73.4	65.5	(dominant) Road traffic noise, birdsong
20/08/2014	13:00	60	0-1	SW	12	70.8	87.5	56.9	73.4	66.1	
						935 A.S. 7			W		AND AND A

PARSONS BRINCKERHOFF

M80 Noise Survey Report

				Job Numb	~				3513048C		
;) ust)				JOD NUME	ier:				33130460		
quipment: NA-28									Adam Price		
Pre-Calibration Level: 94.0 dB						scription:			Mix of clear skies and overcast		
93.9 dB		Date:							20/08/2014		
od		Weather			Statistica	al Noise Le	evels / dB				
me Elapsed Minutes	Wind Speed (m/s)	Wind Direction (from)	Temperat ure (°C)	L _{Aeq}	L _{Amax}	L _{Amin}	L _{A10}	L _{A90}	Description of Audible Noise		
Williaces	(m/s)	(from)									
) 60	(m/s) 0-1	SW	12	77.0	86.9	62.1	80.0	69.9			
			12 12	77.0 77.4	86.9 87.3	62.1 61.6	80.0 79.9	69.9 71.2	(dominant) Road traffic noise, birdsong		
i	NA-28 94.0 dB 93.9 dB iod Elapsed	NA-28 94.0 dB 93.9 dB iod Elapsed Wind Speed	NA-28 94.0 dB 93.9 dB iod Weather Elapsed Sneed Direction	NA-28 94.0 dB 93.9 dB iod Weather Elapsed Wind Wind Temperat	NA-28 94.0 dB 93.9 dB iod Elapsed Sneed Direction Temperat	NA-28 94.0 dB 93.9 dB iod Elapsed Sneed Direction Temperat	NA-28 94.0 dB 93.9 dB iod Elapsed Sneed Direction Elapsed Sneed Mind Mind Sneed Direction Temperat Lass L	NA-28 94.0 dB 93.9 dB iod Weather Elapsed Speed Direction Temperat	NA-28 94.0 dB 93.9 dB iod Weather Statistical Noise Levels / dB Elapsed Sneed Direction Temperat		







ANNEX C

CALIBRATION CERTIFICATES



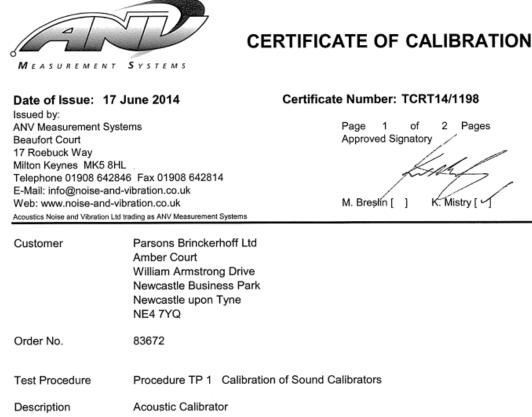
MEASUREMENT	SYSTEMS	, CERTIFIC	ATE OF C	ALIBRATION
Date of Issue: 18	June 2014	Certific	ate Number: T	CRT14/1201
Issued by: ANV Measurement Syste Beaufort Court 17 Roebuck Way	ems		Page 1 Approved Signa	of 2 Pages atory
Milton Keynes MK5 8HL Telephone 01908 64284 E-Mail: info@noise-and- Web: www.noise-and-vik Acoustics Noise and Vibration Ltd t	6 Fax 01908 6428 vibration.co.uk pration.co.uk		M. Breslin []	K. Mistry [
Customer	Parsons Brinck Amber Court William Armstra Newcastle Bus Newcastle upor NE4 7YQ	ong Drive iness Park		
Order No. Description	83672 Sound Level M	eter / Pre-amp / Micropl	hone / Associated	d Calibrator
Identification	<i>Manufacturer</i> Rion Rion Rion Rion	Instrument Sound Level Meter Firmware Pre Amplifier Microphone Calibrator Calibrator adaptor ty	<i>Type</i> NA-28 NH-23 UC-59 NC-74	Serial No. / Version 00380778 1.8 70703 00940 35173440 NC-74-002
Performance Class Test Procedure	1 TP 2.SLM 6167 Procedures from			e periodic tests
Type Approved to IEC	61672-1:2002 If YES above the	Yes Approva	I Number 2 [.] the SLM has succe	1.21/07.01
Date Received	applicable patter 13 June 2014	n evaluation tests of IEC 6 AN		RAC14/06106

The sound level meter submitted for testing has successfully completed the class 1 periodic tests of tec 61672-3:2006, for the environmental conditions under which the tests were performed. As public evidence was available, from an independent testing organisation responsible for approving the results of pattern evaluation tests performed in accordance with IEC 61672-2:2003, to demonstrate that the model of sound level meter fully conformed to the requirements in IEC 61672-1:2002, the sound level meter submitted for testing conforms to the class 1 requirements of IEC 61672-1:2002.

Previous Certificate	Dated	Certificate No.	Laboratory
	19 June 2012	TCRT12/1069	ANV Measurement Systems
This certificate provides	traceability of measuren	nent to recognised nation	hal standards, and to units of measurement
realised at the National	Physical Laboratory or ot	her recognised national	standards laboratories. This certificate may
not be reproduced other	than in full, except with the	ne prior written approval o	of the issuing laboratory.

Pages





Identification Manufacturer Instrument Model Serial No. NC-74 35173440 Rion Calibrator

The calibrator has been tested as specified in Annex B of IEC 60942:2003. As public evidence was available from a testing organisation (PTB) responsible for approving the results of pattern evaluation tests, to demonstrate that the model of sound calibrator fully conformed to the regirements for pattern evaluation decribed in Annex A of IEC 60942:2003, the sound calibrator tested is considered to conform to all the class 1 requirements of IEC 60942:2003.

ANV Job No.	TRAC14/06106	
Date Received	13 June 2014	
Date Calibrated	17 June 2014	
Previous Certificate	Dated Certificate No. Laboratory	12 June 2013 TCRT13/1218 ANV Measurement Systems

This certificate provides traceability of measurement to recognised national standards, and to units of measurement realised at the National Physical Laboratory or other recognised national standards laboratories. This certificate may not be reproduced other than in full, except with the prior written approval of the issuing laboratory.



APPENDIX C – NOISE MODELLING ASSUMPTIONS & TRAFFIC DATA

M80 DBFO STEPPS to HAGGS Checklist								
Which noise modelling software was used, including version?	Cadna A, Version 4.4.145							
What prediction methodology was used?	CRTN							
What deviations from the prediction methodology were adopted?	None, however see free field or façade note below.							
What search radius was used?	2000m							
What number of reflections was used?	Cadna A has been set up to apply 'Reflection via Correction', and therefore compliant with CRTN. Not reflections via mirrored sources. Yes (Low-Traffic-Correction from Chart 12 in CRTN)							
Has low flow correction been used? How is ground absorption included in the model?	A ground absorption of 0.5 had been set. This describes the variation in soft ground (rural areas) and hard ground (urban areas) in the model.							
If a default ground absorption has been used what value was used?	0.5 (globally)							
If default heights for buildings were adopted, what	Exact heights for buildings beyond (North of) Auchenkilns junction were used. South of Auchenkilns junction the same default value of 8m was used. Google Earth was used to spot check heights of buildings. New buildings not included in the previous models (5 in total) were							
heights were used?	manually inputted and heights were estimated using Google street view images. 2.5m added to height for each additional storey.							
If used, what absorption coefficients were used?	Cadna A has been set up to apply Reflection via Correction. Not reflections via mirrored sources.							
What source height and location was adopted?	Following CRTN. 0.5m above the carriageway and 3.5m within the outside edge of the carriageway.							
Are noise levels free field or façade?	Free field, (façade correction applied in analysis)							
If noise contour grids have been produced, what grid spacing has been used and what height?	10m by 10m grid spacing has been used at a height of 4m							
If receptor points have been located at buildings, what distance from the building are they? And how have their locations around buildings been determined.	Set 1m from façade of building, using a Cadna tool.							

If acoustic barriers included in the model, what reflectivity/absorption was used?	Cadna A has been set up to apply 'Reflection via Correction', and therefore compliant with CRTN. Not reflections via mirrored sources.
How have modelling attributes/values that lie out with the range of validity of the prediction method been dealt with?	CRTN has been validated to 600m and all calculations were within 600m.
State all model simplifications or assumptions	See attached assumptions table from previous report with updates
made.	where necessary. Previous models provided the topography/mapping for 2012.
What data sources have been used to create the ground models (include supplier, file name and version)? What data sources have been used for the source input data (include supplier, file name and version)?	For 2008 a detailed digital terrain model provided was used file name: 'Survey_Nat_3D' (06/08/14) for mapping and all of the vertical alignment except for the Auchenkilns Junction section which was taken from the previous model (the same alignment as 2012). For 2003 topo data provided was used in conjunction with 2012 data. Road traffic data for 2012 was acquired from HMG. 2008 and 2003 from other sources. See traffic assessment below.
What digital mapping data has been used (e.g OS MasterMap), and where and when was it sourced?	See ground models section.
What data was used to identify addresses?	Address point database from HMG.
If acoustic barrier information supplied, what was the source and what version was included in the model?	Acoustic barrier information for 2012 and 2008 was provided by the project team. The info was also verified using Google Earth.
If proprietary mapping data was used (e.g. OS Mastermap, please provide licensing information)?	OS mapping provided by the project team.
What other datasets were used to create the noise models, provide details of the source of data, and what it was used for?	N/A

Cadna Modelling assumptions

	Data concerned	Sub category of data	description	date
1	Building Height Data		Building heights from previous model (northern section), used for overlap section Auchenkilns junction. All building height data for previous model (Southern Section) set to 8m.	17-Ap
			Action: used satellite images as well as google street view to verify heights in both North section and South section.	
2	Topography		Topographic data from the previous models was used for the 2012 model, the vertical alignment of the roads for the 2003 model was provided seperately.	Apr
2	Topography		Action: The 2003 model, used the vertical alignment of the road provided and then used 2012 topographic data for the surroundings. It was deemed no significant changes in topography had	Арі
			Action: The 2003 model, used the ventical alignment of the road provided and then used 2012 topographic data for the surroundings. It was deemed no significant changes in topography had occurred in these surrounding areas.	
			update Action 01/09/14: The 2008 model topographic data has been provided by HMG. This was subsequently found to be 2003 vertical alignment and so a 2008 topo datset was constructed	
			by combining the 2003 alignment with the Auchenkilns Junction section from the 2012 model	Auc
3	Road Widths		Road widths are missing in Northern section of the model (2012). and all sections in 2003.	Ma
			Action: for consistency we used the same widths as used in southern section model (RQ15.5-motorway(3lane), RQ 14 (2lane) and RQ10 for slip & minor roads) and verified with google earth.	
		1	update Action 01/09/14: The same action but applied to 2008 model.	1
Δ	Noise Barriers 2003 & 2008		We understand from HMG, that it is not possible to confirm the location or existance of any noise barriers implement in the year 2003.	
-+	110130 Darriers 2003 & 2000		Action: No barriers were implemented in our 2003 model including the central reservation barrier.	28-N
			<u>update Action 01/09/14:</u> New information on the 2008 model barrier locations provided by HMG. They detailed barrier locations around the Auchenkilns junction, no barrier locations were	28-1
			detailed for the rest of the scheme and so no other barriers were implemented into 2008 model.	
5	Noise Barriers 2012		Acoustic barrier information for 2012 was provided by HMG.	
5	Noise Damers 2012		Action noise barriers for our 2012 model were verified using satellite images and as part of the noise survey.	
			September 2014 Action: advice followed: Where traffic speed is < 75 km/h surface correction is -1.0 dB(A) for all roads and all scenarios.	
			Where traffic speed is >= 75km/h:	
,			Pre-Construction scenarios (2003&2008): surface correction is 0 dB(A) unless there are any roads identified as low noise surfaces in which case the surface correction is -2.5 dB(A).	
6	Road Surface		Post-construction scenarios: surface correction is 0 dBA except for road surfaces identified as low noise surfaces:	
			For new low noise surfaces at the time of opening (2008 for Auchenkilns section, 2012 for the rest of the M80): surface correct -3.5 dB(A) *(see update);	
			For low noise surfaceing in future scenarios (2012 for Auchenkilns section): surface correction is -2.5 dB(A).	Se
			location of low noise surfaces provided on as Built drawings.	
			*update Action10/14: From draft report comments PB has been advised that the 2008 Auchenkilns section should be given a surface correction of -2.5dB(A)	
7	Traffic data			
		Road speeds	Speed data not provided for 2012 (unable to extract from data, there are significant gaps).	Au
			Action: Use CRTN road classification in chart 4 section 14.2 for all years.	
		Traffic flows	Section of Roads absent in 2012 or 2003, for example the A80 section Hornshill roundabout to Crow wood roundabout.	AL
			Action: unless the section of road appears in both years (2012&2003) it was left out of both.	
			update Action 01/09/14: Roads were extrapolated from (2003/2008/2012) to provide the most complete model possible	
8	Presentation of Results			1
		Receptor heights	Bungalows (1 floor dwellings) were not easily identifiable.	12th
			Action: In the assessment the worst case scenario of every property having at least 1 storey (a 1st floor) was taken. For all high rise buildings a calculation was done for each floor. All elligible properties were manually checked using google earth street view and if there were bungalows the first floor receptor was removed.	



Project Name:	M80 DBFO Noise Mo	delling		
Project Number:	3513048B			
Technical Note Number:	01			
Technical Note Title:	Traffic Estimation Me	ethodology		
Status / Issue Number:	Issue 1	Date Issued:	22 August	2014
Prepared By:	MSR	Checked by:	FR	Issued by: RP

1. INTRODUCTION

1.1. Study Outline

- 1.1.1. Parsons Brinckerhoff has been commissioned by Bilfinger RE Asset Management Ltd to undertake acoustic analysis along the M80 corridor near Cumbernauld. Part of the study required the assessment of conditions in 2008 prior to construction of the central Stepps to Haggs section of the motorway.
- 1.1.2. Traffic counts from 2008 were not available for all the sections of highway covered by this assessment and therefore some estimation of likely traffic levels was necessary.

1.2. Document Structure

- 1.2.1. This note details the data sources and methodology employed in the calculation of these traffic estimates and is structured as follows:
 - Section 2 Traffic Estimation Methodology;
 - Section 3 Summary.

2. TRAFFIC ESTIMATION METHODOLOGY

2.1. Preamble

2.1.1. This section details the supporting data and assumptions used in the estimation of the likely traffic levels in the Cumbernauld area in 2008.

2.2. Available Data Sources

- 2.2.1. Traffic data for the study area, provided by Transport Scotland, gave the volume of vehicles recorded on various sections of the Cumbernauld area highway network in 2003, 2008 and 2012. The traffic data had been collected and was presented in a variety of ways and levels of detail, ranging from classified hourly counts to daily average flow volumes.
- 2.2.2. The traffic estimates required for the acoustic analysis were 18hr Annual Average Weekday Traffic (AAWT) flows along with the corresponding proportion of heavy goods vehicles (HGVs) for each section of highway in the study area. Where the 18hr AAWT for 2008 had been surveyed and recorded, this was used.

2.3. Estimation Methodology

- 2.3.1. As data for 2008 was not available for all sites, a hierarchy of potential alternatives was defined to ensure that the source with the highest confidence level was used in each case.
- 2.3.2. The available data was employed for the estimation process in the following order:
 - 2008 Original target year;
 - 2003 Same network as the target year;
 - 2012 Different network following completion of construction work.
- 2.3.3. In the cases where data from an alternative year was used, the recorded volume has been factored to estimate the likely volume in 2008. The scaling factor for each of the links missing from the 2008 data set has been calculated from the recorded flows on adjacent links. In some cases, this factoring method was also used to convert flows presented as 24hr AAWT or Annual Average Daily Traffic (AADT) flows into the required form.
- 2.3.4. Some M80 slip-roads where adjacent surveys were not available have been estimated using the flow on the slip road carrying the opposing movement to the same location, for example the traffic volume leaving the motorway to access an industrial estate is assumed to be the same volume leaving the estate and re-joining the motorway.
- 2.3.5. The proportion of HGVs on the missing links was also estimated by combining the observed value from the selected alternative year with the change in HGV proportion between the alternative and target years at an adjacent count site with data covering both years.
- 2.3.6. For a smaller number of sites there was also no data available for 2012 or 2003, the same estimation process was followed as above for these sites.

2.4. Highway Network Coverage

2.4.1. The highway network extending into the area surrounding the M80 corridor has been assumed to carry traffic volumes observed at count sites adjacent to the motorway.

2.5. Limitations

- 2.5.1. As the wider highway network extends past junctions away from the survey location, the estimates become subject to progressively higher margins of error.
- 2.5.2. Estimating traffic flows from volumes recorded in other years is dependent on the assumption that travel patterns are broadly similar across the intervening period, with any changes in traffic volumes occurring uniformly across the study area. As the time difference between the observed and estimated traffic volume increases, the probability of changing travel patterns causing a significant change in traffic flow volume steadily rises.

2.6. Data presentation

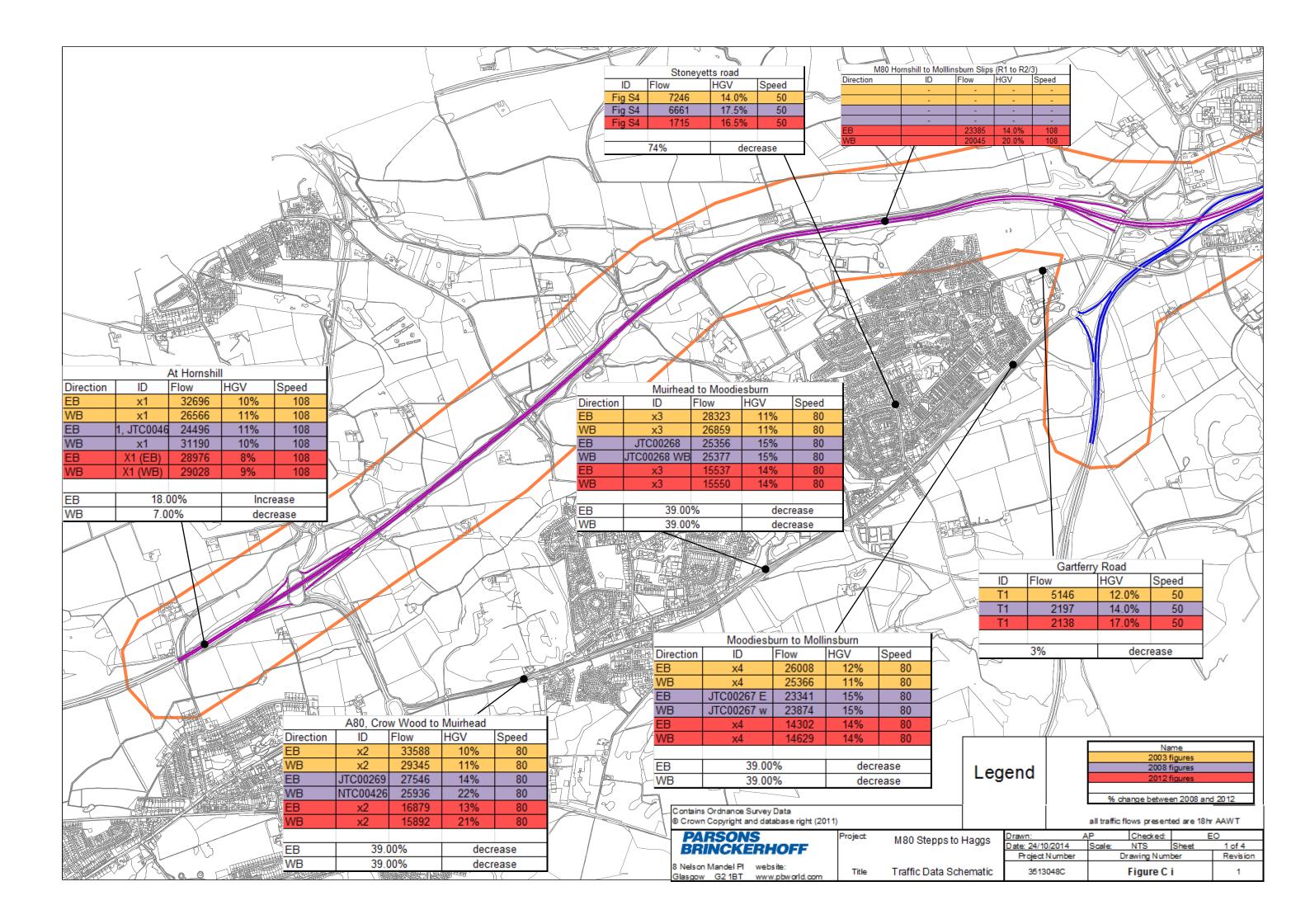
2.6.1. All traffic data used in this study has been presented in the traffic data table. Traffic data estimates are highlighted in orange. The main links of the M80 scheme have also been presented in a traffic data figure.

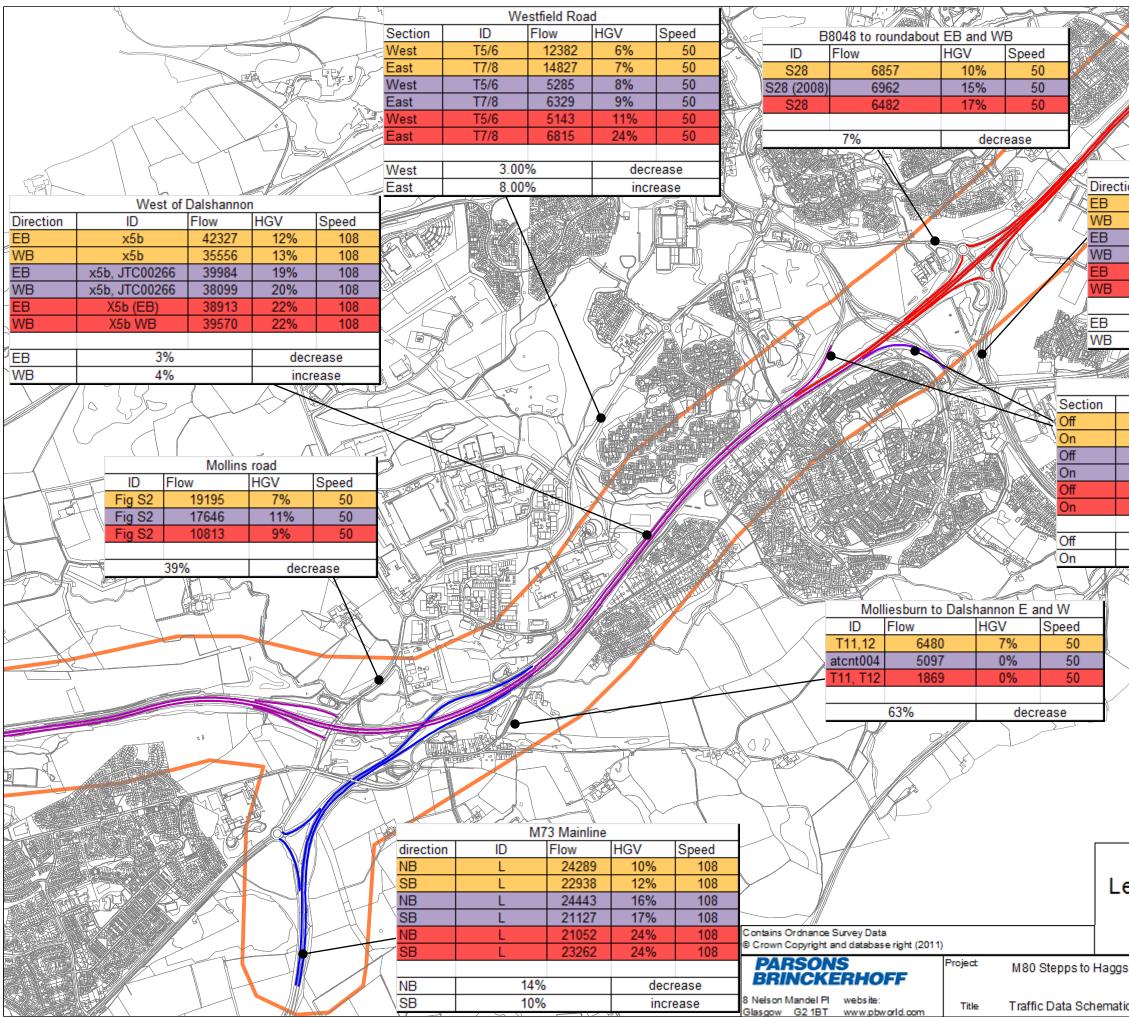
3. SUMMARY

3.1.1. This note summarises the methodology employed in estimating the 2003, 2008 and 2012 traffic levels along the M80 corridor for use in acoustic analysis.

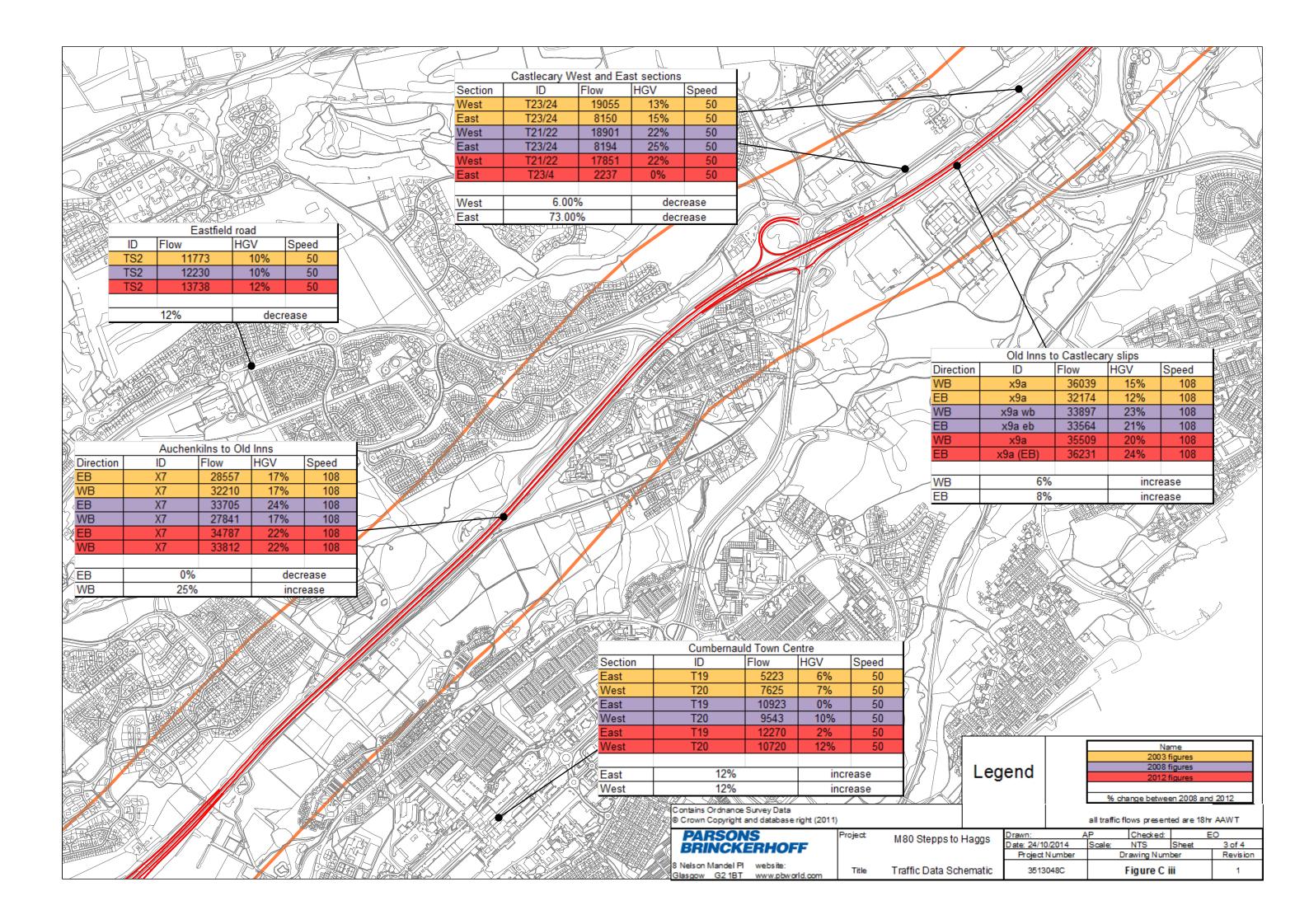
Road Traffic Data Table

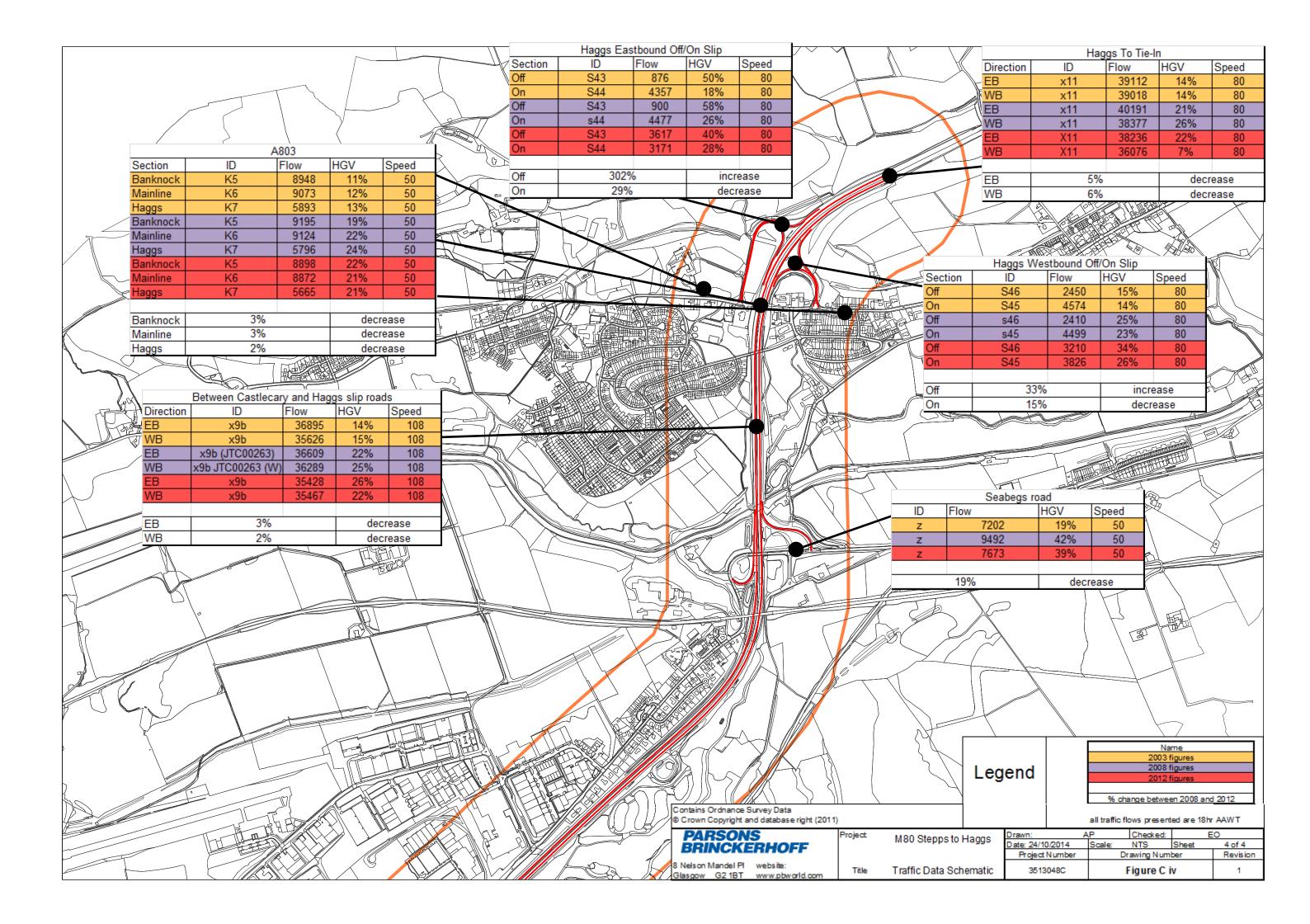
2003 road name	ID	A AWT 19hr flow	HGV percentage Speed KF	H 2008 road name	ID	A AWT 19br flow	HGV percentage	Speed KBU	2012 road name		AWT 19br flow	HGV percentage	peed KPH Percentage chan	go with 20128 2008	Comments
At Hornshill E	x1	32696	10% 1	08 M80 Between A80 and Jct 3 S or E	x1, JTC00468	24496	11%	108	M80 0459N M 11/2 mile N,R1 to R2	X1 (EB)	28976	8%	108	18	Commenta
At Hornshill W	x1	26566	11% 1	08 At Hornshill W 08 M80 Between A80 and Jct 3 N or W	x1	31190	10%	108	M80 0459S M 11/4 mile N,R1 to R3 (west) 1	X1 (WB)	29028	9%	108	-7	
A80, M80 Crow Wood to Hornshill West of Dalshannon EB	A80, M8000024 x5b	19929 42327	13% 1 12% 1	08 M80 Between A80 and Jct 3 N or W 08 (M80) A80 East of M73 Junction	JTC00468 x5b, JTC00266	24198 39984	11% 19%	108 108	M80 Between A80 and Jct,S3 to S4 + S4 to S3 M80 W of J5 Auchenkilns,R1 to R2	A80, M8000024 X5b (EB)	10731 38913	6% 22%	108	-56	Link to Crow Wood Roundabout changes to off ramp in 2012
West of Dalshannon WB	x5b	35556	13% 1	08 (M80) A80 East of M73 Junction	x5b, JTC00266	38099	20%	108	M80 1425S M W of J5 Au,R1 to R3 (west) 7	X5b WB	39570	22%	108	4	
Low wood Slip to Auchenkilns WB Low wood slip to Auchenkilns EB	x6 x6	27098 27521		08 (M80) Low wood slip to Auchenkilns WB 08 Low wood Slip to Auchenkilns EB	x6	26229	20%	108	M80 1473S M J5 Auchenk,R1 to R3 (west) 7 M80 1473N M J5 Auchenk,R4 to R66	x6 WB	33294 29637	26% 32%	108 108	27	
Auchenkilns to Oldd Inns EB	X7	28557	17% 1	08 (M80) A80 East of Auchinkilns Rbt EB	X7	33705	24%	108	M80 E of J5 Auchenkilns, M80 Eastbound	X7	34787	22%	108	0	
Auchenkilns to Old Inns WB between old inns slips WB	X7 x8 WB	32210 32809		08 A80 East of Auchinkilns Rbt WB 08 (M80) between old inns slips wb	X7	27841	17%	108	M80 1833S M W of J6 Ol,M80 Westbound M80 1883S M J6 Old Inn.M80 Westbound	X7 X8	33812 29534	22%	108	25	
between old inns slips WB between old inns slips EB	X8 WB	32809		08 (M80) between old inns slips wb 08 between old inns slips EB	x8 WB (2008) X8	31462 35759	22%	108	M80 1883S M J6 Old Inn,M80 Westbound M80 1892N M J6 Old Inn.M80 Eastbound	X8	29534 28780	26%	108	-6 -20	
Old inns to Castlecary slips wb	x9a	36039		08 (M80) A80 Cumbernauld to Castlecary (WB)	x9a wb	33897	23%	108	M80 2138S M W of J6a C,M80 Westbound	x9a	35509	20%	108	6	
Old Inns to Castle cary slips eb between Castlecary and Haggs slip roads EB	x9a x9b	32174 36895		08 A80 Cumbernauld to Castlecary (EB) 08 (M80) A80 South of M80 Junction 4	x9a eb x9b (JTC00263)	33564 36609	21% 22%	108	M80 W of J6a Castlecary,M80 Eastbound M80 2187N M J6a Castle,M80 Eastbound	x9a (EB) x9b	36231 35428	24% 26%	108 108	-1	
Between Castlecary and Haggs slip roads WB	x9b	35626	15% 1	08 A80 South of M80 Junction 4	x9b JTC00263 (W)	36289	25%	108	M80 2187S M J6a Castle, M80 Westbound	x9b	35467	22%	108	-2	
Between Haggs Slips WB	x10	34750		08 (M80) Between Haggs Slips EB	x10	40549 36373	21%	108	M80 2297N M J7 Haggs, M80 Eastbound	x10	32490	28%	108	-19 -11	
Between Haggs Slips EB Haggs slip road (E) to tie-in EB	x10 x11	34445 39112		08 Between Haggs Slips WB 08 (M80) Haggs slip road (E) to tie-in EB	x10 x11	40191	26% 21%	108	M80 2297S M J7 Haggs,M80 Westbound M80 E of J7 Haggs,M80 Eastbound	x10 X11	32866 38236	22% 22%	108 108	-11	
Haggs slip road (E) to tie-in WB	x11	39018	14% 1	08 Haggs slip road (E) to tie-in WB	x11	38377	26%	108	M80 Haggs Westbound	X11	36076	7%	108	-6	
A73 to roundabout Nth bound A73 to roundabout SB	\$33 \$33	4601 5268		A73 to roundabout Nth bound 60 A73 to roundabout SB	S33 S33	4671 5348	28%	<u>60</u> 60	A73 to roundabout Nth bound	\$33 \$33	5251 6012	32% 30%	60	12	
Low wood off slip	S25	14453	5% 8	30 Low wood off slip	S25	13989	9%	80	M80 1428NO O Off slip,R18 to 19	\$25	7819	2%	80	-44	
Low wood On Slip Old Inns E/B Diverge slip	\$26 \$34	7711 3336		Low wood On Slip Old Inns E/B Diverge slip	\$26 \$34	8192 3708	12% 38%	80 80	M80 1473SI I On slip a,R20 to R21 M80 1892NO O Off slip ,Old Inns Eastbound Off S	S26 S34	7370 4135	14% 26%	80 80	-10	
Old Inns E/B Diverge slip Old Inns E/B merge slip	\$34 \$35	6980		Old Inns E/B Diverge slip 80 Old Inns E/B merge slip	\$34 \$35	7760	9%	80	M80 1892NO O Off slip ,Old Inns Eastbound Off S M80 1903NI I On slip a,Old Inns Eastbound On SI	\$34 \$35	6005	20%	80	-23	
Haggs E/B diverge slip	\$43	876	50% 8	80 Haggs E/B diverge slip	S43	900	58%	80	M80 2297NO O Off slip ,Haggs Eastbound Off Slip	S43	3617	40%	80	302	attributed to growth in Haggs
M80 2297NI I On slip a,Haggs Eastbound On Slip Haggs Westbound On Slip	S44 S45	4357 4574	18% 8	Haggs E/B merge slip Haggs w/b merge slip	<u>s44</u> s45	4477 4499	26%	80	M80 2297NI I On slip a,Haggs Eastbound On Slip Haggs Westbound On Slip	S44 S45	3171 3826	28% 26%	80	-29	
M80 2297SO O Off slip ,Haggs Westbound Off Slip	S46	2450	15% 8	BO Haggs W/B Diverge slip Haggs W/B Diverge slip	s46	2410	25%	80	M80 2297SO O Off slip ,Haggs Westbound Off Slip	S46	3210	34%	80	33	
North road T17, T18	T17/18 T11.12	4682 6480	10% 5	North road T17, T18 UCL MAIN ROAD CONDORRAT, Main Road West	T17/18 atcnt004	3683 5097	3% 0%	50	North Road S19 to S20 + S20 to S19 UCL MAIN ROAD CONDORRAT, Main Road West	T17,18 T11, T12	1146 1869	7% 0%	50	-69 -63	
Molliesburn to Dalshannon E and W Dalshannon to Condorrat E and W	T13,14	6480 7242	6%	OUCL MAIN ROAD CONDORRA I, Main Road West Dalshannon to Condorrat E and W (2008)	T13,14	5697	0%	50 50	Dalshannon to Condorrat E and W (2008)	T13,14	2033	0%	50	-63	+
Main road condorrat	use T17,18 ∶ 2012	2954	10% 5	0 Main road condorrat	use T17,18 ∶ 201	2 2323	3%	50	Main Road East	T17a and 18a	723	7%	50	-69	
Mollinsburn WB Merge Mollinsburn WB diverge	C	13558 713		Mollinsburn WB Merge Mollinsburn WB diverge	C	13644 718	12%	80	M73 2062SI I On slip a,R62 to R63 M73 2062SO O Off slip,R64 to R65	C	2259 2798	0%	80 80	-83 290	Layout and changes in road network
M73 Mainline NB	L	24289	10% 1	08 M73 Mainline SB	L	24443	16%	108	M73 1962(N) M W of J3,R52 to R53 +R53 to R52	Ľ	21052	24%	108	-14	
M73 Mainline SB B8048 to roundabout EB and WB	L \$28	22938 6857		08 M73 Mainline NB 50 B8048 to roundabout EB and WB	L \$28 (2008)	21127	17%	108	M73 1962(S) M W of J3,R52 to R53 +R53 to R52	L	23262	24%	108	10	
Westfield road West	528 T5/6	12382		Westfield road West	T5/6	5285	8%	50 50	Westfield road West	528 T5/6	6482 5143	17%	50	-7 -3	+
Westfield road East	T7/8	14827		0 Westfield road East	T7/8	6329	9%	50	Westfield road East	T7/8	6815	24%	50	8	
Mollins road A80, Crow Wood to Muirhead EB	Fig S2 x2	19195 33588		Mollins road 30 A80 West of Muirhead	Fig S2 JTC00269	17646 27546	11% 14%	50 80	Mollins road A80 West of Muirhead	Fig S2	10813 16879	9% 13%	50 80	-39 -39	
A80, Crow Wood to Muirhead WB	x2	29345	11% 8	A80 25W M at J3 Crowwood Rbt	NTC00426	25936	22%	80	A80 25W M at J3 Crowwood Rbt	×2	15892	21%	80	-39	
Muirhead to Muirhead EB Muirhead to Muirhead WB	x2a	27864		A80 West of Muirhead	JTC00269	27145	15%	80	A80 West of Muirhead	x2a	16633 16560	14%	80	-39	
Muirhead to Muirhead WB Muirhead to Moodiesburn EB	x2a x3	26763 28323		A80 MUIRHEAD WB A80 Muirhead to Moodiesburn	JTC00150 WB JTC00268	27026	15% 15%	80 80	A80 MUIRHEAD WB A80 Muirhead to Moodiesburn	x2a x3	16560	14% 14%	80	-39 -39	
Muirhead to Moodiesburn	x3	26859	11% 8	A80 Muirhead to Moodiesburn WB	JTC00268 WB	25377	15%	80	A80 Muirhead to Moodiesburn WB	x3	15550	14%	80	-39	
Moodiesburn to Mollinsburn EB Moodiesburn to Mollinsburn	x4 x4	26008 25366		A80 West of M73 Junction 30 A80 West of M73 Junction	JTC00267 E JTC00267 w	23341 23874	15% 15%	80 80	A80 West of M73 Junction A80 West of M73 Junction	x4 x4	14302 14629	14% 14%	80	-39 -39	
Gartferry Road	T1	5146		60 Gartferry Road	T1	23074	14%	50	Gartferry Road	T1	2138	14%	50	-39	
Stoneyetts road	Fig S4	7246	14%	50 Stoneyetts road	Fig S4	6661	18%	50	Stoneyetts road	Fig S4	1715	17%	50	-74	data taken from ES figure, as no other data provided
Lindsaybeg Road Mollinsburn	S8 T9,T10	4661 7095	10% 5	60 Lindsaybeg Road 60 Mollinsburn	58 T9,T10	4285	14% 4%	50	Lindsaybeg Road Mollinsburn	T9,T10	1103 2046	13% 0%	50	-74 -63	
Cumbernauld Town Centre E	T19	5223	6%	0 Cumbernauld Town Centre E	T19	10923	0%	50	Cumbernauld Town Centre E	T19	12270	2%	50	12	
Cumbernauld Town Centre W	T20 T23/24	7625 19055	7% 5	Cumbernauld Town Centre W Castlecary West	T20	9543	10%	50	Cumbernauld Town Centre W Castlecary West	T20	10720	12% 22%	50	12	
Castlecary West Castlecary east E	T23/24	8150	15%	60 Castlecary east E	T23/24	8194	25%	50	Castlecary east E	T23/4	2237	0%	50	-73	
Castlecary S25/26	Transport Scot	4001 11773	26%	60 Castlecary S25/26	S25/26	8034	33%	50	B816 CASTLECARY ROAD, S25 to S26 New Castlecar		3037	4%	50	-62	
Eastfield road Seabegs road	152	7202	10% 5	60 Eastfield road 60 Seabegs Overbridge	TS2	12230	10%	50	Eastfield road Seabegs Overbridge	TS2 7	13/38	12%	50	-19	
A803 Banknock	K5	8948	11% 5	0 A803 Banknock	K5	9195	19%	50	A803 Banknock	K5	8898	22%	50	-3	
A803 Mainline A803 Haggs	K6 K7	9073 5893	12% 5 13% 5	60 A803 Mainline 60 A803 Haggs	K6 K7	9124 5796	22% 24%	50	A803 Mainline	K6	8872	21%	50	-3	
Castlecary E/B or N/B merge slip	S40	3427		Koos haggs Castlecary junction NB	S40	3488	51%	80	M80 2187NI I On slip a,Castlecary Eastbound On	S40	952	22%	80	-73	
Offslip/diverge Castlecary W/B or S/B	\$42	3578	8% 8	0 Offslip Castlecary SB	S42	3505	18%	80	M80 2187SO O Off slip ,Castlecary Westbound Off	\$42	978	24%	80	-72	
Auchengeich road	\$21/22	2608	12% 5	60 Auchengeich road	S21/22	2398	16%	50	Auchengeich road	S21/22	874	23%	50 note: positive m	-64 leans an increase in flows	
roads/sections not comparable in all years				roads/sections not comparable in all years					roads/sections not comparable in all years				Percentage chan	ge with 2012& 2008]
West of Lowwood EB	ID x5c	AAWT 18hr flow 42327	HGV percentage Speed KF 12% 1	VH 08 (M80) West of Lowwood EB	ID x5c	AAWT 18hr flow 38985	HGV percentage Spe	ed KPH 108	R52 to R53 +R53 to R52 (M73 between slips)		AWT 18hr flow 38923	HGV percentage Speed 32%	108	N/A	+
West of Lowwood WB	x5c x5c	34798		08 (M80) West of Lowwood EB 08 West of Lowwood WB	x5C x5C	38985	20%	108	R52 to R53 +R53 to R52 (M73 between junc)	between slips between junc	38923 38462	32%	108	N/A N/A	Not comparable sections of road, due to road layout changes
(M80) East of Mollinsburn EB	x5a	42329		08 East of Mollinsburn EB (M80)	x5a	38987	17%	108	M73 2062S M M73 J3 to ,R56 to R57	x5a	17410	28%	108	N/A	
(M80) East of Mollinsburn WB A80, M80 on slip at Hornshill	x5a A80, M8000057	35556 26566		08 (M80) East of Mollinsburn WB 30 A80 MOODIESBURN (SB)	x5a JTC00149 (S)	35782 24987	19% 15%	108 80	M73 2060N M M73 J3 to ,R54 o R55 A80 MOODIESBURN	x5a	21052 3756	30% 14%	108 80	N/A N/A	Not comparable sections of road, due to road layout changes
Overbridge @ Hornshill	S4	6637	1% 8	0 Overbridge @ Hornshill (2008)	S4	6992	5%	80	R12 to R13	Hornsrdbt	6937	4%	50	N/A	with no other available data, the WSP model was used.
Old Inns W/B East merge slip Old Inns W/B East diverge slip	\$36 \$37	713 5416		Old Inns W/B East merge slip 00 Old Inns W/B East diverge slip	S36 S37	684 5194	7% 12%	80 80	M80 629SO O Off slip a,R12 to R13 M80 629NI I On slip at,R10 to R11	HornsOffWB Horns OnEB	2679 2337	18% 19%	80	N/A N/A	
Mollinsburn FB diverge	b	978	5% 8	Mollinsburn EB diverge	b	901	10%	80	M80 1124NO O Off slip ,R14 to R15		3237	18%	80	N/A	
Mollinsburn EB Merge	B	8651	9% 8	80 Mollinsburn EB Merge	B	7968	14%	80	M80 1124SI I On slip a, R16 to R17		3282	15%	80	N/A	
Old Inns W/B West merge slip Old Inns W/B West diverge slip	K36 K37	550 3100	3% 8 9% 8	0 Old Inns W/B West merge slip 0 Old Inns W/B West diverge slip	K36 K37	579 3266	11% 17%	80	M73 2001NI I On slip a,R60 to R61 M73 1977NO O Off slip ,R58 to R59	+ +	7525 4220	34% 22%	80	N/A N/A	+
Castlecary W/B or S/B merge slip	S41	3427	43% 8	Castlecary junction W/B or S/B merge	S41	3488	52%	80	M80 1883SI I On slip a,Old Inns Westbound On SI	\$36	4083	24%	80	N/A	
				A80 MOODIESBURN (NB) Auchenkilns Offslip EB	JTC00149 (N)	24890	15.0%	80	M80 1938SO O Off slip ,Old Inns Westbound Off S	\$37 \$77	5795	19%	80	N/A -3	<u> </u>]
				M80 Auchenk, EB between slips	377	28016	20%	108	M80 1551Ni T On slip a,R26 ti R25 M80 1541N M J5 Auchenk,R4 to R66	3.0	28066	20%	108	0	+
				M80 1551NI I On slip a,R26 ti R27 EB		4308	2%	80	M80 1551NI I On slip a,R26 ti R27	Aucha	4446	0%	80	3	
				M80 1528SI I On slip a,R24 ro R25 M80 between WB slips Auchenk		3592	14%	80	M80 1528SI I On slip a,R24 ro R25 M80 1541S M J5 Auchenk,R5 to R66 (west)	Auchen slip	3731 29406	16% 22%	80 108	4	+
				M80 1551SO O Off slip ,R28 to R29		3428	9%	80	M80 1551SO O Off slip ,R28 to R29		4163	14%	80	21	
				A80 MUIRHEAD junction	JTC00150	27268	15%	80	M80 1124N M J4 Mollins,R1 to R2 M80 578S M J3 Hornshil,R1 to R3 (west) 1	↓	19571	20%	108	N/A N/A	
									M80 578S M J3 Hornshil,R1 to R3 (west) 1 M80 673S M E of J3 Hor,R1 to R3 (west) 1	+ +	20045 22816	20%	108 108	N/A N/A	+
									M80 1124S M J4 Mollins,R1 to R3 (west) 7		19644	16%	108	N/A	
									S4 to S3 S3 to S4	Crow to Horns Horns to Crow	3721 5126	2%	50	N/A N/A	with no other available data, the WSP model was used. with no other available data, the WSP model was used.
									M80 578NO O Off slip a,R6 to R7 (Horns EB)	xi	9566	14%	80	N/A	
									M80 578SI I On Slip at, R8 to R9 Hornshill (WB) Hornshill Roundabout	xii	9838 6207	10%	80	N/A N/A	with no other available data, the WSP model was used.
									A80 MUIRHEAD junction	+ +	6207 9944	3%	50 80	N/A N/A	with no other available data, the WSP model was used.
KEY									M80 578N M J3 Hornshil,R1 to R2		20150	5%	108	N/A	
KET															
Extrapolated data: data from ES figure									M80 W of J4 Mollinsburn,R1 to R2	part of x5a	23385 21342	14% 24%	108 108	N/A N/A	





		X26886C747// >4.11111			
ion		ID	Flow	HGV	Speed
		S33	4601	23%	60
		S33	5268	21%	60
	_	S33	4671	28%	60
		S33 S33	5348 5251	26% 32%	60 60
		S33	6012	30%	60
		000	0012	0070	00
		12%		incre	ase
		12%		incre	ase
	Lo	w Wood slip	S S		
	ID	Flow	HGV	Speed	
	S25	14453	5%	80	
	S26	7711	5%	80	
	S25	13989	9%	80	
	S26 S25	8192 7819	12% 2%	80 80	
	S25	7370	14%	80	4 2
	020	1510	1 1470	00	$\leq R^{-1}$
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	44°			rease rease	
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	end	%	decr 20 20 20 20 20 20 20 20 20 20 20 20 20	Pease Name 03 figures 08 figures 12 figures ween 2008 and ented are 18 hr	AAWT
eg	end	% 	decr decr 20 20 20 20 20 20 20 20 20 20 20 20 20	Pease Name 03 figures 08 figures 12 figures 12 figures ented are 18 hr dented are 18 hr	AAWT
	end	% all tr AP D/2014 Sca Number	decr decr 20 20 20 20 20 20 20 20 20 20 20 20 20	Pease Name 03 figures 03 figures 12 figures	AAWT







APPENDIX D – ES NOISE SENSITIVE RECEPTORS

Property		Pre-construction year 2008 (dB)	ES, 2010 Scheme with mitigation (dB)	PB 2012 Post construction levels (dB)	(PB 2012 - PB 2008) difference (dB)	(PB 2012 Model - ES 2010 with mit) difference (dB)
Hornshill	G	67.0	63.3	60.5	-6.5	-2.8
	1st	68.5	64.0	61.7	-6.8	-2.3
South Broomknowes	G	53.8	54.5	54.0	0.2	-0.5
	1st	54.6	54.8	54.8	0.2	0.0
Drumsack Farm	G	57.8	62.6	58.4	0.6	-4.2
	1st	58.2	63.5	60.2	2.0	-3.3
Peathill Farm	G	46.7	58.6	58.4	11.7	-0.2
	1st	48.4	60.1	59.5	11.1	-0.6
Greenlea Cottage North	G	63.6	63.9	59.6	-4.0	-4.3
Davidston Mains Farm	G	51.6	62.7	62.2	10.6	-0.5
	1st	52.2	64.9	62.7	10.5	-2.2
Crow Wood House	G	74.8	66.4	72.4	-2.4	6.0
	1st	75.8	68.7	73.5	-2.3	4.8
12 Church Road	G	78.0	64.0	75.1	-2.9	11.1
	1 st	79.2	66.0	76.3	-2.9	10.3
13 Dunellan Avenue	G	71.4	60.1	69.1	-2.3	9.0
	1st	72.6	62.0	70.3	-2.3	8.3
Braeside Farm	G	51.0	64.0	59.3	8.3	-4.7
	1st	52.6	65.1	61.0	8.4	-4.1
24 Stoneyetts Cottages	G	51.5	61.0	63.0	11.5	2.0
	1st	51.8	63.1	63.8	12.0	0.7
Bowling Green, Stoneyetts (FF)	G	49.2	58.5	56.1	6.9	-2.4
5 The Cuillins	G	44.5	62.5	59.0	14.5	-3.5
	1st	47.6	63.8	60.7	13.1	-3.1
15 The Larches	G	42.2	61.3	59.0	16.8	-2.3
	1st	45.1	63.8	62.5	17.4	-1.3
15 Croftmoraig Avenue	G	45.4	58.1	56.6	11.2	-1.5
U	1st	48.5	60.1	58.2	9.7	-1.9
Deerdykes Cottage	G	70.7	73.5	68.8	-1.9	-4.7
1 Cumbernauld Road	G	71.6	64.8	64.0	-7.6	-0.8
	1st	73.0	69.0	67.7	-5.3	-1.3
Mollinsburn Rec Area (FF)	G	68.0	67.7	64.4	-3.6	-3.3
Rosebank	G	71.5	67.6	63.4	-8.1	-4.2
	1st	72.2	68.5	64.5	-7.7	-4.0

		_				
Property		Pre-construction year 2008 (dB)	ES, 2010 Scheme with mitigation (dB)	PB 2012 Post construction levels (dB)	(PB 2012 - PB 2008) difference (dB)	(PB 2012 Model - ES 2010 with mit) difference (dB)
Badenheath Park,Mollinsburn	G	72.6	72.9	64.0	-8.6	-8.9
1 Craigend Road	G	77.8	72.1	66.3	-11.5	-5.8
	1 st	79.6	72.5	68.6	-11.0	-3.9
67 Craigend Road	G	65.0	63.7	57.2	-7.8	-6.5
0	1 st	66.4	64.3	58.7	-7.7	-5.6
Deerdykes Car Park (FF)	G	68.3	70.9	65.2	-3.1	-5.7
116 Main Road, Dalshannon	G	78.3	67.0	65.8	-12.5	-1.2
,	1 st	80.6	71.0	68.4	-12.2	-2.6
14 Gainburn Gardens	G	67.1	70.7	60.3	-6.8	-10.4
	1 st	68.4	70.8	61.4	-7.0	-9.4
4 Woodmill Gardens	G	73.7	65.5	63.6	-10.1	-1.9
	1st	76.8	69.2	66.1	-10.7	-3.1
Westfield Industrial Area	G	73.1	80.4	70.7	-2.4	-9.7
3 Main Road	G	63.2	68.3	59.2	-4.0	-9.1
	1st	64.5	69.6	60.6	-3.9	-9.0
5 Craigelvan Court	G	79.1	66.0	65.0	-14.1	-1.0
	1st	79.9	67.6	66.5	-13.4	-1.1
16 Leckethill Court	G	67.9	62.3	63.2	-4.7	0.9
	1st	68.4	63.3	63.7	-4.7	0.4
7 Craigelvan View	G	75.3	64.2	63.9	-11.4	-0.3
0	1st	76.0	65.3	65.0	-11.0	-0.3
28 Leckethill Avenue	G	66.2	63.3	62.8	-3.4	-0.5
	1st	67.0	64.2	63.6	-3.4	-0.6
14 Leckethill View	G	58.9	60.5	56.7	-2.2	-3.8
	1st	61.2	62.2	58.9	-2.3	-3.3
1 Summerfield Road	G	66.5	69.2	60.2	-6.3	-9.0
	1 st	67.3	69.3	61.1	-6.2	-8.2
Playground at Westfield (FF)	G	66.9	63.5	64.0	-2.9	0.5
26 Kirkview	G	63.6	65.6	57.8	-5.8	-7.8
	1 st	65.4	65.7	58.6	-6.8	-7.1
19 Craigside Place	G	56.2	59.4	53.8	-2.4	-5.6
17 Inchwood Court	G	68.8	63.4	62.3	-6.5	-1.1
	1st	71.9	64.9	64.3	-7.6	-0.6
20 Inchwood Road	G	69.1	63.8	65.5	-3.6	1.7
	1st	73.9	69.6	71.6	-2.3	2.0
48 Inchwood Road	G	70.4	64.5	64.9	-5.5	0.4
	1st	71.5	65.9	66.4	-5.1	0.5
St Francis of Assisi School	G	64.7	59.2	59.9	-4.8	0.7
27 Kirk Place	G	77.9	66.7	67.8	-10.1	1.1
	1 st	79.6	69.5	70.1	-9.5	0.6
39 Main Road	G	69.0	70.9	63.0	-6.0	-7.9
	1 st	69.5	71.5	64.2	-5.3	-7.3
Library, Condorrat	G	68.5	62.9	62.8	-5.7	-0.1
15 Rosehill Drive	G	74.2	66.3	63.5	-10.7	-2.8
	1st	74.9	68.2	64.6	-10.3	-3.6

_		Pre-construction year 2008 (dB)	ES, 2010 Scheme with mitigation (dB)	PB 2012 Post construction levels (dB)	(PB 2012 - PB 2008) difference (dB)	(PB 2012 Model - ES 2010 with mit) difference (dB)
Property		70.4	07.5	01.0	0.0	0.7
21 Rosehill Drive	G	73.1	67.5	64.8	-8.3	-2.7
Noveido Cottogo	1st G	74.8	70.2	66.5	-8.3	-3.7
Vayside Cottage	-	67.9	64.9	66.6	-1.3	1.7
	1st	76.8	76.7	75.9	-0.9	-0.8
t Maurices High School	G G	60.1	55.0	59.5	-0.6	4.5
0 Maree Drive		61.8	69.3	60.7	-1.1	-8.6
	1st G	63.0	69.8	62.0	-1.0	-7.8
6 Maree Drive	-	55.2	60.8	55.2	0.0	-5.6
	1st G	57.3	62.4	57.3	0.0	-5.1
a Main Road	-	62.5	65.5	59.6	-2.9	-5.9
9 Maree Drive	G	64.6	63.7	64.4	-0.2	0.7
Morar Court	1st	65.9	65.4	65.9	0.0	0.5
Moral Court	G 1 st	64.8	63.6	63.3	-1.5	-0.3
		66.6	65.7	65.3	-1.3	-0.4
1 Auchenkilns Holdings	G	65.0	63.3	64.4	-0.6	1.1
	1st	66.3	65.2	65.6	-0.7	0.4
9 Grangeneuk Gardens	G	61.2	60.0	61.2	0.0	1.2
	1st	61.8	60.5	61.7	-0.1	1.2
3-85 Southfield Road	G	63.3	62.6	63.1	-0.2	0.5
	1st	64.0	63.1	63.8	-0.2	0.7
5 Southfield Road	G	64.5	66.1	64.4	-0.1	-1.7
	1st	65.3	66.6	65.0	-0.3	-1.6
1a Southfield Road	G	68.3	67.4	67.8	-0.5	0.4
	1st	69.0	68.4	68.4	-0.6	0.0
7/19 Southfields	G	68.9	66.3	67.9	-1.0	1.6
	1st	72.6	69.0	72.0	-0.6	3.0
owling Green, Ravenswood (FF)	G	65.3	66.5	64.5	-0.8	-2.0
2 Langdales Avenue	G	65.7	61.4	62.0	-3.7	0.6
	1st	66.8	62.4	62.7	-4.1	0.3
0 Berryhill Road	G	66.8	66.1	66.6	-0.2	0.5
	1 st	67.9	66.7	67.7	-0.2	1.0
11 Binniehill Road	G	69.8	65.2	66.4	-3.4	1.2
	1 st	70.5	66.3	67.3	-3.2	1.0
8 Binniehill Road	G	63.3	60.1	61.4	-1.9	1.3
	1 st	66.3	61.7	63.9	-2.4	2.2
2 Binniehill Road	G	61.0	57.7	58.0	-3.0	0.3
	1 st	64.3	59.3	60.7	-3.6	1.4
0 Binniehill Road	G	60.2	58.1	57.2	-3.0	-0.9
	1 st	63.2	59.2	57.2	-3.4	0.6
1d Braeface Road	G 1 st	68.9	65.8	67.4	-1.5	1.6
		69.6	67.1	67.9	-1.7	0.8
9 Binniehill Road	G	63.7	62.3	61.2	-2.5	-1.1
	1 st	64.8	63.4	62.3	-2.5	-1.1
03 Craighalbert Rd	G	70.2	62.4	66.4	-3.8	4.0
	1 st	71.2	63.6	67.5	-3.7	3.9

Proporty		Pre-construction year 2008 (dB)	ES, 2010 Scheme with mitigation (dB)	PB 2012 Post construction levels (dB)	(PB 2012 - PB 2008) difference (dB)	(PB 2012 Model - ES 2010 with mit) difference (dB)
Property Zoar Cottage	G	76.4	67.5	71.1	-5.3	3.6
	1 st	77.1	69.3	73.0	-4.1	3.7
19h Braeface Road	G	65.9	61.5	62.7	-3.2	1.2
	1 st	66.7	62.8	63.5	-3.2	0.7
Seafar	G	77.7	70.0	71.3	-6.4	1.3
	1 st	78.4	70.7	72.3	-6.1	1.6
39 Allanfauld Road	G	66.9	63.3	63.6	-3.3	0.3
	1 st	69.0	64.5	65.5	-3.5	1.0
53 Hayston Road	G	68.2	64.5	65.7	-2.5	1.2
o hayston road	1 st	68.4	64.9	66.0	-2.4	1.1
2 Callander Court	G	68.6	64.1	66.3	-2.3	2.2
	1 st	68.9	65.2	66.6	-2.3	1.4
39 Landsdowne Drive	G	67.8	61.2	64.5	-3.3	3.3
	1 st	69.2	62.9	65.8	-3.4	2.9
8 - 118 The Auld Road	G	66.7	61.9	62.8	-3.4	0.9
	1 st	68.9	63.7	64.4	-3.9 -4.5	0.9
	2 nd	71.0		64.4	-4.5 -5.3	-
	2 3 rd		65.1			0.6
		72.9	66.9	67.0	-5.9	0.1
5 The Auld Road	G 1 st	77.8	68.3	72.3	-5.5	4.0
		81.4	74.4	75.4	-6.0	1.0
Lansdowne Drive	G 1 st	69.8	62.4	64.9	-4.9	2.5
		72.9	64.1	67.6	-5.3	3.5
1 Letham Grange	G	62.3	56.2	58.8	-3.5	2.6
	1 st	64.6	57.7	60.5	-4.1	2.8
4 Letham Grange	G	60.9	55.8	57.3	-3.6	1.5
	1 st	63.2	56.6	59.1	-4.1	2.5
' Nairn Way	G	58.0	56.0	55.8	-2.2	-0.2
	1 st	60.1	55.7	57.5	-2.6	1.8
1 Carrick Road	G	74.2	64.9	66.8	-7.4	1.9
	1 st	78.2	67.7	69.7	-8.5	2.0
Cumbernauld Old Parish Church	G	66.2	57.6	60.1	-6.1	2.5
	1 st	67.7	58.9	61.4	-6.3	2.5
Recreation Area & Car Park (FF)	G	72.0	58.6	63.0	-9.0	4.4
36 Roadside Cumbernauld	G	74.6	60.6	64.2	-10.4	3.6
	1 st	79.1	62.5	66.6	-12.5	4.1
26 Roadside, Cumbernauld	G	69.2	58.7	61.8	-7.4	3.1
	1 st	72.1	60.6	64.4	-7.7	3.8
3 Dornoch Way	G	71.9	64.4	68.3	-3.6	3.9
	1 st	73.7	65.7	70.0	-3.7	4.3
4 Muirfield Road	G	67.6	71.1	63.5	-4.1	-7.6
	1 st	69.6	72.8	64.7	-4.9	-8.1
9 Roadside, Cumbernauld	G	71.1	69.2	64.3	-6.8	-4.9
	1 st	72.1	69.9	65.3	-6.8	-4.6
25 Smithyends	G	59.0	56.9	56.4	-2.6	-0.5
	1 st	62.1	59.8	59.2	-2.9	-0.6
13 Muirfield Road	G	70.0	64.4	65.0	-5.0	0.6
	1 st	70.7	65.2	65.7	-5.0	0.5

Dranortu		Pre-construction year 2008 (dB)	ES, 2010 Scheme with mitigation (dB)	PB 2012 Post construction levels (dB)	(PB 2012 - PB 2008) difference (dB)	(PB 2012 Model - ES 2010 with mit) difference (dB)
Property 1 Westerwood Rise	G	69.4	68.7	64.0	-5.4	-4.7
	1 st	70.7	69.9	65.5	-5.2	-4.4
22/24 Rigghead Avenue	G	72.3	71.0	63.3	-9.0	-4.4
22/24 Riggliead Avenue	1 st		73.4	65.2	-9.3	-8.2
		74.5				
Dobbies Garden Centre	G G	75.1	72.2	70.8	-4.3	-1.4
2 Roadside, Cumbernauld	1 st	68.9	71.5	63.8	-5.1	-7.7
Mand Davis North Industrial Estate		71.2	71.8	65.0	-6.2	-6.8
Ward Park North Industrial Estate	G	73.3	75.8	70.5	-2.8	-5.3
Filling Station, Old Inns	G	77.2	79.5	73.9	-3.3	-5.6
Ward Park South Industrial Area	G	77.0	76.8	72.9	-4.1	-3.9
Ward Park Ind Area 2	G	71.2	67.5	67.0	-4.2	-0.5
Ward Park Ind Area 3	G	76.8	80.4	72.2	-4.6	-8.2
Ward Park Ind Area 4	G	81.4	68.2	77.7	-3.7	9.5
2a Castlecary Road	G 1 st	80.5	72.2	71.7	-8.8	-0.5
		81.8	78.0	75.6	-6.2	-2.4
8a Castlecary Road	G	79.2	70.0	72.1	-7.1	2.1
	1 st	80.3	73.9	75.1	-5.2	1.2
Castlecary Castle	G	68.7	66.0	64.5	-4.2	-1.5
	1 st	69.2	66.4	64.8	-4.4	-1.6
6 Castle Court	G	77.5	68.6	68.2	-9.3	-0.4
	1 st	79.4	72.0	71.0	-8.4	-1.0
28 Castle Court	G	79.2	72.4	71.2	-8.0	-1.2
	1 st	80.5	76.6	73.9	-6.6	-2.7
Glenside Cottage	G	78.1	70.3	69.6	-8.5	-0.7
Castra, Walton Road	G	70.8	63.1	66.2	-4.6	3.1
Woodneuk Cottage	G	67.6	56.3	61.6	-6.0	5.3
	1 st	68.6	57.7	62.4	-6.2	4.7
Bridge Keepers Cottage	G	71.6	72.0	66.4	-5.2	-5.6
	1 st	76.2	73.0	71.0	-5.2	-2.0
114 Holy Grove	G	71.6	63.3	66.4	-5.2	3.1
	1 st	72.0	64.7	66.8	-5.2	2.1
1 Cumbernauld Road, Haggs	G	61.0	63.6	58.6	-2.4	-5.0
	1 st	64.0	64.4	63.7	-0.3	-0.7
8 Aunchinloch Drive	G	67.3	61.5	62.5	-4.8	1.0
	1 st	67.7	62.2	63.1	-4.6	0.9
50 Aunchinloch Drive	G	70.2	66.3	65.9	-4.3	-0.4
	1 st	72.8	68.0	69.0	-3.8	1.0
2 Morgorot Avenue	G					
2 Margaret Avenue	1 st	67.6	69.5	63.1	-4.5	-6.4
		68.2	70.5	63.7	-4.5	-6.8
36 Hollandbush Crescent	G 1 st	58.7	57.5	55.9	-2.8	-1.6
		60.0	58.6	57.2	-2.8	-1.4
St Lukes Church	G	67.1	58.1	62.7	-4.4	4.6
74 Auchincloch Drive	G	73.0	69.9	69.2	-3.8	-0.7
	1 st	75.7	70.8	71.4	-4.3	0.6
9 Garngrew Road	G	66.3	70.4	63.0	-3.3	-7.4
	1 st	67.3	71.6	64.3	-3.0	-7.3
Bankview Nursing Home	G	59.7	53.4	57.6	-2.1	4.2
	1 st	62.2	56.1	60.2	-2.0	4.1

